PS403 - Digital Signal processing

IV. DSP - The Z-Transform

Key Text:

Digital Signal Processing with Computer Applications (2nd Ed.)

Paul A Lynn and Wolfgang Fuerst, (Publisher: John Wiley & Sons, UK)

We will cover in this section

How to compute the Z-Transform of a signal/impulse response

Poles and zeros of the Z-Transform of a signal or LTI processor

Frequency analysis using the Z-Transform

Definition:
$$X(Z) = \sum_{n=0}^{\infty} x[n]Z^{-n}$$

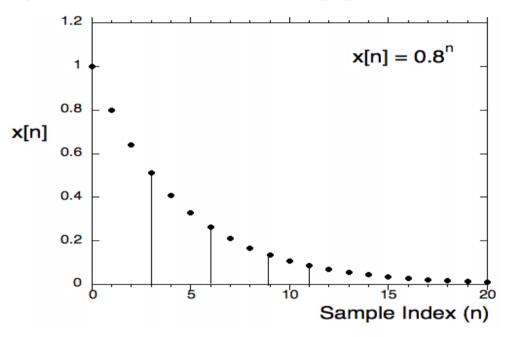
Origins:

The Z-Transform is useful for looking at signals and systems in the frequency domain. It is not unlike the Laplace/Fourier Transforms except that it has its origins in sampled data systems, while Laplace/ Fourier Transforms apply to analog (continuous valued) signals and systems.

X(Z) is NOT concerned with x[n] prior to n = 0; Unilateral $\sum_{n=0}^{\infty}$

X(Z) is effectively a power series in Z^{-1} , with coefficients given by the values of x[n].

Example: Find the Z-T of $x[n] = 0.8^{\circ}, 0.8^{1}, 0.8^{2}, 0.8^{3},...$



$$X(z) = 1xZ^{0} + 0.8xZ^{-1} + 0.64xZ^{-2} + 0.512xZ^{-3} +$$

= $1+(0.8xZ^{-1})^{1}+(0.8xZ^{-1})^{2}+(0.8xZ^{-1})^{3}+...$

$$\Rightarrow X(Z) = \frac{1}{1 - 0.8Z^{-1}} = \frac{Z}{Z - 0.8}$$

Example: Find the signal x[n] with Z-Transform: $X(Z) = \frac{1}{Z+1.2}$

$$X(Z) = \frac{1}{Z+1.2} = \frac{Z^{-1}}{1+1.2.Z^{-1}}$$

$$= Z^{-1} (1 + 1.2Z^{-1})^{-1}$$

$$= Z^{-1} \left[1 + \left(-1.2Z^{-1} \right)^{1} + \left(-1.2Z^{-1} \right)^{2} + \left(-1.2Z^{-1} \right)^{3} + \dots \right]$$

$$= 1Z^{-1} - 1.2Z^{-2} + 1.44Z^{-3} + \dots$$

Coeff of Coeff of x[1] x[2] x[3]

By inspection:

$$x[0] = 0$$

$$x[1] = 1$$

$$x[2] = -1.2$$

$$x[3] = 1.44$$

$$x[n] = (-1.2)^{n-1}$$

- 1. Notice that although both signals theoretically contain an infinite number of sample values, their Z-Ts are very compact
- 2. One can think of the of Z as a time-shift operator Multiplication by $Z \equiv \text{time advance}$ by one sampling interval Division by $Z \equiv \text{time delay}$ by one sampling interval

Example: Time shifting a unit impulse

The Z-T of a unit impulse is given by:

$$X(Z) = \sum_{n=0}^{\infty} \delta[n] Z^{-n} = Z^{-n} \Big|_{n=0} = 1$$

The Z-T of a unit impulse delayed by n₀ sampling intervals is:

$$X(Z) = \sum_{n=0}^{\infty} \delta[n - n_0] Z^{-n} = Z^{-n} \Big|_{n=n_0} = Z^{-n_0}$$

Hence time shifting in Z-space becomes a simple operation - multiplication by Z^{n_0} for time delay or Z^{+n_0} for time advance

As the Z-T & F-T are related, the convolution theorem applies!

$$X(Z) = \sum_{n=0}^{\infty} x[n] Z^{-n} \text{ , let } Z = \exp(j\Omega)$$

$$\Rightarrow X(\Omega) = \sum_{n=0}^{\infty} x[n] \exp(-jn\Omega)$$

If x[n] is an input signal and h[n] a processor response; we know that:

$$y[n] = x[n]*h[n]$$

and hence

$$Y(\Omega) = X(\Omega).H(\Omega)$$

and
 $Y(Z) = X(Z).H(Z)$

Convolution Theorem applies to Z-Ts

Convolution Theorem - proof by example

Direct convolution: y[n] = h[n]*x[n]

n	0	1	2	3	4	5	6	7	8
x[n]	1	-2	3	-1	-1	0	0	0	0
h[n]	2	1	-1	0	0	0	0	0	0
y[n]	2	-3	3	3	-6	0	1	0	0

Z-T Multiplication: Y(Z) = H(Z).X(Z)

$$X(Z) = \sum_{n=0}^{\infty} x[n]Z^{-n}$$
 $X(Z) = 1 - 2Z^{-1} + 3Z^{-2} - Z^{-3} - Z^{-4}...$
 $H(Z) = 2 + Z^{-1} - Z^{-2}$

$$Y(Z)=H(Z).X(Z)=2-3Z^{-1}+3Z^{-2}+3Z^{-3}-6Z^{-4}+0Z^{-5}+Z^{-6}=\sum_{n=0}^{\infty}y[n]Z^{-n}$$

By inspection: $y[n] = 2, -3, 3, 3, -6, 0, 1, 0, 0, \dots$

A processor has an impulse response in Z-space given by:

$$H(Z) = \frac{1}{Z(Z-1)(2Z-1)}$$

Find the (i) corresponding difference equation describing the action of the processor and (ii) its impulse response.

(i) find y[n]

$$H(Z) = \frac{1}{Z(Z-1)(2Z-1)} = \frac{Y(Z)}{X(Z)}$$

$$\Rightarrow Y(Z)[Z(Z-1)(2Z-1)] = X(Z)$$

$$2Z^{3}Y(Z) - 3Z^{2}Y(Z) + ZY(Z) = Y(Z)$$

Since multiplication by Z is \equiv time advance by one sampling interval we can write:

$$2y[n+3] - 3y[n+2] + y[n+1] = x[n]$$

Since this is a simple recurrence formula we can let $n \rightarrow n-3$ without any loss of generalisation

$$\Rightarrow$$
2y[n] - 3y[n-1] + y[n-2] = x[n-3]
or

$$y[n] = 1.5y[n-1] - 0.5y[n-2] + 0.5x[n-3]$$

Show that h[n] = 0, 0, 0, 0.5, 0.75, 0.875,...

We can now study more complex processors, e.g.,

$$H(Z) = \frac{Z^2(Z-1)(Z^2+1)}{(Z+0.8)(Z^2+1.38593Z+0.9604)(Z^2-1.64545Z+0.9025)} = \frac{Y(Z)}{X(Z)}$$

$$[Z^5 - Z^4 + Z^3 - Z^2].X(Z) = [Z^5 + 0.54048Z^4 - 0.62519Z^3 - 0.66354Z^2 + 0.60317Z + 0.69341].Y(Z)$$

$$x[n+5] - x[n+4] + x[n+3] - x[n+2] =$$
 $y[n+5] + 0.54048y[n+4] - 0.62519 y[n+3] - 0.66354y[n+2]$
 $+ 0.60317y[n+1] + 0.69341y[n]$

Since we can let $n \rightarrow n-5$ without any loss of generalisation

$$y[n] = -0.54048y[n-1] + 0.62519 y[n-2] + 0.66354y[n-3] - 0.60317y[n-4] - 0.69341y[n-5] + x[n] - x[n-1] + x[n-2] - x[n-3]$$

Steady State Response of a Processor - Final Value Theorem

Step Response S[n] as 'n' gets very large!

If
$$x[n] \frac{Z - Transform}{\Rightarrow} X(Z)$$

$$\Rightarrow \frac{Lim}{n \to \infty} x[n] = \frac{Lim}{Z \to 1} \left(\frac{Z - 1}{Z}\right) X(Z)$$

Note that the Z-T of a unit step $\mathbf{u[n]} = \frac{Z}{Z-1}$

Hence if u[n] is an input signal to a system with transfer function H(Z), then the output signal is given by:

$$Y(Z) = \left(\frac{Z}{Z-1}\right)H(Z)$$

Final Value Theorem

$$\Rightarrow \frac{Lim}{n \to \infty} S[n] = \frac{Lim}{Z \to 1} \left(\frac{Z - 1}{Z}\right) Y(Z)$$

$$= \frac{Lim}{Z \to 1} \left(\frac{Z - 1}{Z}\right) \left(\frac{Z}{Z - 1}\right) H(Z) = \frac{Lim}{Z \to 1} H(Z)$$

Finally the Final Value Theorem States that:

$$\frac{Lim}{n \to \infty} S[n] = \frac{Lim}{Z \to 1} H(Z)$$

Final Value Theorem: Example

Consider
$$y[n] = 0.8y[n-1] + x[n]$$

Then
$$h[n] = 0.8h[n-1] + \delta[n]$$

and
$$H(Z) = \frac{Z}{Z - 0.8}$$

Ergo

$$\frac{Lim}{n \to \infty} S[n] = \frac{Lim}{Z \to 1} H(Z) = \frac{1}{1 - 0.8} = 5$$

Look back at step response of this processor in section 3

Frequency Analysis using Z-Transforms

$$X(Z) = \sum_{n=0}^{n=\infty} x[n]Z^{-n}$$

Substituting $Z = \exp(j\Omega)$

$$\Rightarrow X(\Omega) = \sum_{n=0}^{n=\infty} x[n] \exp(-jn\Omega)$$

The Z-Transform is most useful not just for compact description of LTI processors with long/infinite impulse reponse but also for inferring their frequency response

Poles and zeros of X(Z):

X(Z) is always a rational function, i.e., it can always be written as a ratio of two polynomials in Z.

Hence on can write:

$$X(Z) = \frac{N(Z)}{D(Z)} = K \cdot \frac{(Z - Z_1)(Z - Z_2)(Z - Z_3).....}{(Z - P_1)(Z - P_2)(Z - P_3).....}$$

Where $Z_1, Z_2,....$ are the Zeros of X(Z) and $P_1, P_2,....$ are the Poles of X(Z)

If $x[n] \in R \Rightarrow Poles \& Zeros$ are either real or occur in complex conjugate pairs

Z-Plane and the Argand Diagram:

It is often useful to plot the poles and zeros of a Z-T on an Argand diagram. In fact, a trained eye will deduce the salient features of a processor response from the plot quite easily!

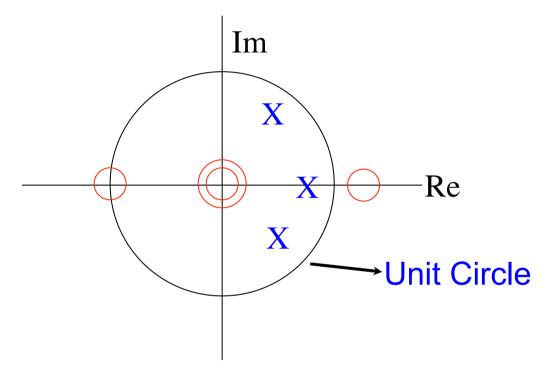
Convention

Zeros are plotted as \bigcirc symbols Poles are plotted as X symbols

Example: Plot the poles and zeros of the following ZT:

$$X(Z) = \frac{Z^2(Z-1.2)(Z+1)}{(Z-0.5+j0.7)(Z-0.5-j0.7)(Z-0.8)}$$

Example: Poles and zeros



By inspection we have:

Zeros @ Z=0 (2 of), Z=1.2 & Z=-1.0 &

Poles @ Z = 0.8, Z = 0.5-j0.7 & Z = 0.5+j0.7

Inferring LTI System Stability from Pole-Zero Plots

Consider a digital LTI processor with ZT: $H(Z) = \frac{Y(Z)}{X(Z)}$

Clear that Y(Z) {and concomitantly the processor output y[n]} determines the location of all zeros of the ZT and that X(Z) and {hence x[n]} determines the locations of the poles.

Say that
$$H(Z) = \frac{Y(Z)}{X(Z)} = \frac{1}{Z - \alpha}$$

System has no zeros and one pole at Z = α

$$ZY(Z) - \alpha Y(Z) = X(Z)$$

$$\Rightarrow y[n+1] - \alpha y[n] = x[n]$$

$$\Rightarrow y[n] = \alpha y[n-1] + x[n-1]$$

Find h[n]!

$$H(Z) = \frac{Y(Z)}{X(Z)} = \frac{1}{Z - \alpha}$$

$$\Rightarrow$$
 h[n] = α h[n-1] + δ [n-1]

$$\Rightarrow$$
 h[n] =0, 1, α , α^2 , α^3 , α^4 ,.....

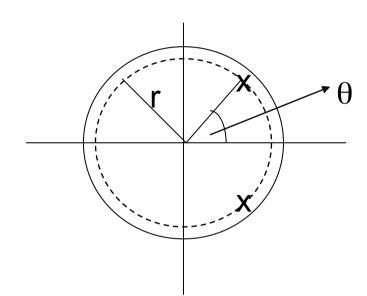
Hence, if α < 1, h[n] may be infinite but at least it is bounded which implies H(Z) describes a stable system.

If $\alpha > 1$, h[n] grows without limit, $\Rightarrow H(Z) = \text{unstable system}$.

Conclusion: A system is stable only if the poles (i.e., all poles) lie within the unit circle!

Clearly the same is true of signals: one or more poles outside the unit circle ⇒ unbounded signal

Pole locations in Polar Coordinates



Two poles lying on a circle of radius 'r' making and angle θ w.r.t the Re(al) axis \Rightarrow So pole locations are r.[exp(j θ)] and r.[exp(-j θ)]

So
$$H(Z) = \frac{Y(Z)}{X(Z)} = \frac{1}{[Z - r.\exp(j\theta)][Z - r.\exp(-j\theta)]}$$
$$= \frac{1}{(Z^2 - 2rZCos\theta + r^2)}$$

Pole locations in Polar Coordinates

$$\Rightarrow Y(Z) \cdot (Z^2 - 2rZCos\theta + r^2) = X(Z)$$

$$\Rightarrow y[n] = 2rCos\theta y[n-1] - r^2y[n-2] + x[n-2]$$

For a bounded (finite) output, $r<1 \Rightarrow$ system is stable

Example Application - See figure 4.2 and equation 4.14

$$H(Z) = \frac{Z^2(Z-1)(Z^2+1)}{(Z+0.8)(Z^2+1.38593Z+0.9604)(Z^2-1.64545Z+0.9025)}$$

Two Re Zeros @ Z=0

One Re Pole @ Z=-0.8

One Re Zero @ Z=1

Two Im Zeros @ Z=±j

Pole locations in Polar Coordinates

Now compare;

$$\frac{1}{\left(Z^2 - 2rZCos\theta + r^2\right)} \quad \text{with} \quad \frac{1}{\left(Z^2 + 1.38593Z + 0.9604\right)}$$

$$r^2 = 0.9604 \text{ and } 2r\text{Cos}\theta = -1.38593$$

 $\Rightarrow r = 0.98 \text{ and } \theta = 45^{\circ}$

$$\frac{1}{\left(Z^2 - 1.64545Z + 0.9025\right)}$$
 yields $r = 0.95$ and $\theta = 150^\circ$

Hence the system is stable because ALL r < 1!

Note:

- (a) Comments on system stability apply only to poles and there is no dependence on zeros of the transform
- (b) Zeros at the origin of the Z-plane produce only a time advance or delay but they have no other effect

Consider again:
$$H(Z) = \frac{1}{\left(Z^2 - 2rZCos\theta + r^2\right)}$$
$$\Rightarrow y[n] = 2rCos\theta y[n-1] - r^2y[n-2] + x[n-2]$$

So that y[0] = 0 and y[1] = 0

We can force y[n] to start @ n=0 by using (b) above !

Simply apply the time advance operator 'Z' twice:

$$H'(Z) = Z^2.H(Z)$$

$$\Rightarrow H'(Z) = \frac{Y(Z)}{X(Z)} = \frac{Z^2}{\left(Z^2 - 2rZCos\theta + r^2\right)}$$

$$\Rightarrow (Z^2 - 2rZCos\theta + r^2)Y(Z) = Z^2X(Z)$$

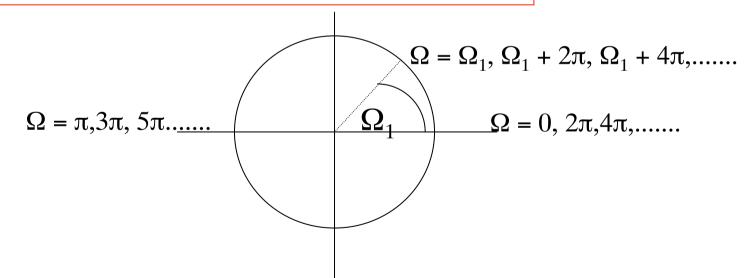
$$\Rightarrow y[n] = 2rCos\theta y[n-1] - r^2y[n-2] + x[n]$$

The Fourier Transform in the Z-Plane: Geometrical Methods

Setting $Z = \exp(-j\Omega)$ we transform the Z-T into the the F-T

Where are the values of $Z = \exp(j\Omega)$ in the Z plane?

Magnitude r = 1; they lie on the unit circle



 Ω_1 = 0 corresponds to the point Z = (1, j0) on the Argand Plane.

As Ω increases, one moves anticlockwise around the unit circle;

@
$$\Omega = \pi$$
, Z = (-1, j0)

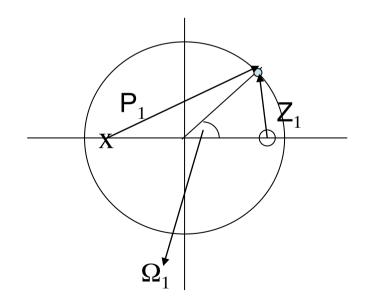
We know from Fourier Analysis that the FT repeats with a period of 2π . The Z-Transform (Z-plane) represention shows this automatically as any one point on the unit circle (1, Ω) can represents all frequencies Ω + $2n\pi$, n= 0, 1, 2, 3, 4,

Consider the following LTI Processor with Z-Transform;

$$H(Z) = \frac{Z - 0.8}{Z + 0.8}$$

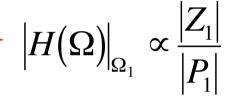
Setting $Z = \exp(j\Omega)$

$$\Rightarrow H(\Omega) = \frac{\exp(j\Omega) - 0.8}{\exp(j\Omega) + 0.8}$$

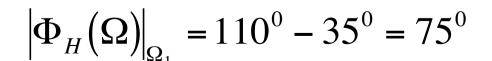


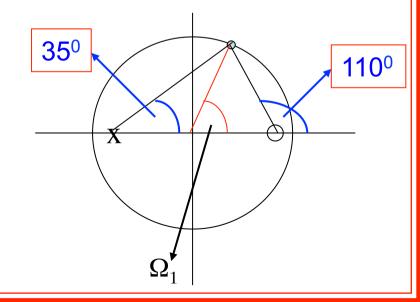
The numerator of H(Z) is determined by the magnitude (length) of the Zero Vector $|Z_1|$ and the denominator by the pole length $|P_1|$.

So the magnitude/gain of the frequency transfer function



The phase shift or phase transfer function





By simple extension of this graphical method one can map the frequency transfer function of a simple processor

Ω	Z ₁	P ₁	H(Ω)
0	0.2	1.8	0.11
$\pi/2$	1.28	1.28	1.00
π	1.8	0.2	9.00
2 π	0.2	1.8	0.11

From figure 4.6 one can see that as one travels around the unit circle (increasing frequency Ω), the gain $|H(\Omega)|$ goes through a maximum when $Z = \exp(j\Omega)$ passes near a pole, here e.g., @ $\Omega = \pi$.

More complex processor- consider again:

$$H(Z) = \frac{Z^2(Z-1)(Z^2+1)}{(Z+0.8)(Z^2+1.38593Z+0.9604)(Z^2-1.64545Z+0.9025)}$$

Zeros @ Z=0 (2nd order), Z =1 and Z = $\pm j$ Poles @ Z = -0.8 {Real, Ω = 180° (π)}, a pole pair close to the unit circle @ Ω = ± 45 ° (π /4) and a second pole pair at Ω = ± 150 ° (5π /6) and also close to the unit circle.

Zeros: Expect 'true nulls' in the frequency response at Ω values specifying their location, here 0 and π

Poles: Expect peaks in the frequency response (gain) at Ω values specifying their location, here $\pi/4$, $5\pi/6$ and π

We can break more complex systems with many zeros and poles into simpler systems as follows:

$$|H(\Omega)| = K \cdot \frac{|Z_1(\Omega)| |Z_2(\Omega)| |Z_3(\Omega)| \dots |Z_3(\Omega)|}{|P_1(\Omega)| |P_2(\Omega)| |P_3(\Omega)| \dots |Z_3(\Omega)|}$$

where K is a constant

$$\Phi_{H}(\Omega) = \left[\Phi_{Z_{1}}(\Omega) + \Phi_{Z_{2}}(\Omega) + \Phi_{Z_{3}}(\Omega) \dots\right] - \left[\Phi_{P_{1}}(\Omega) + \Phi_{P_{2}}(\Omega) + \Phi_{P_{3}}(\Omega) \dots\right]$$

 $\Phi_{Z_n}(\Omega)$ - Phase vector of the nth zero of H(Z)

 $\Phi_{P_n}(\Omega)$ - Phase vector of the nth pole of H(Z)

1st and 2nd order LTI Processors

Any LTI processor
$$H(Z) = K \cdot \frac{(Z - Z_1)(Z - Z_2)(Z - Z_3)...}{(Z - P_1)(Z - P_2)(Z - P_3)...}$$

may be represented by cascading a series of 1st and 2nd order LTI processor transfer functions

1st order
$$H_1(Z) = \frac{(Z - Z_1)}{(Z - P_1)}$$
 Z_1 and $P_1 \in \mathbb{R}$
2nd order $H_2(Z) = \frac{(Z - Z_2)(Z - Z_3)}{(Z - P_2)(Z - P_3)}$

 Z_2 , Z_3 , P_2 , $P_3 \in R$ or occur as complex conjugate pairs

1st and 2nd order LTI Processors - Frequency Selectivity

Poles placed at well defined Ω values (frequencies) and located near the unit circle will produce sharp peaks in the frequency response of a processor. An equal number of zeros placed at the Z-plane origin ensures that h[n] starts @ n=0

We write that a real pole for a 1st order procesor is located at $Z = \alpha$

The complex conjugate pole pair for a 2^{nd} order processor are located at $Z = r.\exp(j\theta)$ and $Z = r.\exp(-j\theta)$

Hence one can write:

$$H_1(Z) = \frac{Z}{(Z - \alpha)}$$

$$H_2(Z) = \frac{Z^2}{\{Z - r.\exp(j\theta)\}\{Z - r.\exp(-j\theta)\}}$$

$$H(Z) = \frac{Z^2}{\left(Z^2 - 2rZCos\theta + r^2\right)}$$

1st order Already looked at these in detail: (see Fig 4.9)

$$0 < \alpha < 1 \Rightarrow$$
 Low pass filter

 $-1 < \alpha < 0 \Rightarrow$ High pass filter

$$H_1(Z) = \frac{Z}{\left(Z - \alpha\right)}$$
, $Z \to \exp(j\Omega) \Rightarrow H_1(\Omega) = H_1(Z)|_{Z = \exp(j\Omega)} = \frac{\exp(j\Omega)}{\exp(j\Omega) - \alpha}$

 $|H_1(\Omega)|$ has a maximum value (or gain) @ $\Omega = 0$

$$G_{\text{max}} = \frac{\exp(j0)}{\exp(j0) - \alpha} = \frac{1}{1 - \alpha}$$

 $|H_1(\Omega)|$ has a minimum value (or gain) @ $\Omega = \pi$

$$G_{\min} = \left| \frac{\exp(j\pi)}{\exp(j\pi) - \alpha} \right| = \frac{1}{1 + \alpha}$$

1st order cont'd

So the closer α is to 1 (i.e., the closer the pole is to the unit circle), the larger the maximium gain (G_{max}), the smaller the minimum gain (G_{min}) and so the narrower the bandwidth of the filter.

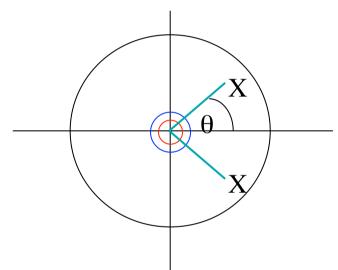
In summary, as one moves the pole of a 1st order filter closer to the unit circle:

- (i) The peak gain increases
- (ii) The bandwidth decreases
- (iii) The impulse response (1, α , α^2 , α^3 , α^4 ,...) slows

(ii) and (iii) ⇒ Narrow the bandwidth and slow the processor

2nd order filters

$$H_2(Z) = \frac{Z^2}{\left(Z^2 - 2rZCos\theta + r^2\right)}$$



The processor has complex conjugate pole pairs @ Z=r.exp(jθ) and a 2nd order zero at the origin (Z=0)

θ determines the centre frequency of the processor /signal and 'r' determines the 'selectivity' or bandwidth

2nd order filters

$$H_2(Z) = \frac{Y(Z)}{X(Z)} = \frac{1}{(1 - 2rCos\theta Z^{-1} + r^2 Z^{-2})}$$

$$\Rightarrow y[n] = 2rCos\theta y[n-1] - r^2y[n-2] + x[n]$$

Letting Z =
$$\exp(j\Omega) \Rightarrow$$

$$H_2(\Omega) = \frac{1}{\left(1 - 2rCos\theta \exp(-j\Omega) + r^2 \exp(-j2\Omega)\right)}$$

Hence:

$$\left|H_{2}(\Omega)\right| = \frac{1}{\left[\left(1 - 2rCos\theta Cos\Omega + r^{2}Cos2\Omega\right)^{2} + \left(2rCos\theta Sin\Omega - r^{2}Sin2\Omega\right)^{2}\right]^{1/2}}$$

Maximum gain occurs at the centre frequency, $\Omega = \theta$.

$$\left|H_{2}(\theta)\right| = G_{\text{max}} = \frac{1}{\left[\left(1 - 2rCos^{2}\theta + r^{2}Cos2\theta\right)^{2} + \left(2rCos\thetaSin\theta - r^{2}Sin2\theta\right)^{2}\right]^{1/2}}$$

Let A=
$$(1-2rCos^2\theta + r^2Cos2\theta)$$

Let B= $(2rCos\thetaSin\theta - r^2Sin2\theta)$ $\Rightarrow G_{max} = \frac{1}{\sqrt{A^2 + B^2}}$

Program 11 used to study the effect of r, θ for 2nd O systems using the expressions above - very powerful - write your own See Figure 4.11 for typical results

Figure 4.11 examples

- (a) Cascaded 1st order LPFs: r = 0.9, max gain @ $\Omega = \theta = 0^0$ (dc)!
- (b) BPF centred @ Ω = θ =25 0 (~15 Samp/cyc.), r=0.99 (narrow passband)
- (c) BPF with wide bandpass (r = 0.8) centred @ Ω = θ =1100 (~3 Samp/cyc.)
- (d) Cacaded 1st order HPFs: r=0.9, max gain @ Ω = θ =1800 (2 Samp/cyc.)

Note: When the pole 'r' value is close to '1', you should also expect rapid variations in the phase transfer function $\Phi_{H}(\Omega)$ as Ω sweeps through the design frequency ' θ '!

Reminder: In sampled data systems we specify 'frequency' in samples/cycles or equivalently 'radians' or 'degrees'!

Effect of initial conditions on the Z - Transform

Useful in two cases:

- (a) The system may not have settled following the application of a prior input
- (b) The input signal was applied prior to n = 0 and it is required to assess its subsequent effects on the output Consider the following:

If: $x[n] \rightarrow X(Z)$

Then: $x[n - n_0] \rightarrow X(Z).Z^{-n_0}$

We can in fact write: $x[n - n_0].u[n - n_0] \rightarrow X(Z).Z^{-n}$

Multiplication by $u[n - n_0]$ ensures that x[n] is zero for $n < n_0$

Suppose that we define $x_1[n]$ as a signal identical to x[n] but not necessarily starting @ n = 0

i.e.,
$$x_1[n] \rightarrow x[n-1]$$

Then: $X_1(Z) = \sum_{n=0}^{n=\infty} x[n-1].Z^n = x[-1] + \sum_{n=1}^{n=\infty} x[n-1].Z^n$

But:
$$\sum_{n=1}^{n=\infty} x[n-1]Z^{-n} = Z^{-1}\sum_{n=1}^{n=\infty} x[n-1]Z^{-(n-1)}$$

And also:
$$Z^{-1} \sum_{n=1}^{\infty} x[n-1] Z^{-(n-1)} = Z^{-1} \sum_{n=0}^{\infty} x[n] Z^{-(n)}$$

So
$$X_1(Z) = x[-1] + Z^{-1} \left\{ \sum_{n=0}^{n=\infty} x[n] Z^{-n} \right\} = x[-1] + Z^{-1}X(Z)$$

Similarly it can be shown that:

If:
$$x_2[n] = x[n - 2]$$

Then:
$$X_2(Z) - x[-2] + x[-1]Z^{-1} + Z^{-2}X(Z)$$

Example - Consider:
$$y[n] = \alpha . y[n-1] + x[n]$$

We can rewrite as:
$$y[n] - \alpha . y[n-1] = x[n]$$

Taking ZTs:
$$Y(Z) - \alpha \left\{ y[-1] + Z^{-1}Y(Z) \right\} = X(Z)$$
$$\Rightarrow Y(Z) \left\{ 1 - \alpha . Z^{-1} \right\} = X(Z) + \alpha . y[-1]$$
$$\Rightarrow Y(Z) = \frac{X(Z) + \alpha . y[-1]}{\left(1 - \alpha . Z^{-1} \right)}$$

Case in point:

$$y[-1] = -\frac{1}{\alpha}$$
 $x[n] = \delta[n]$ $\Rightarrow X(Z) = 1$

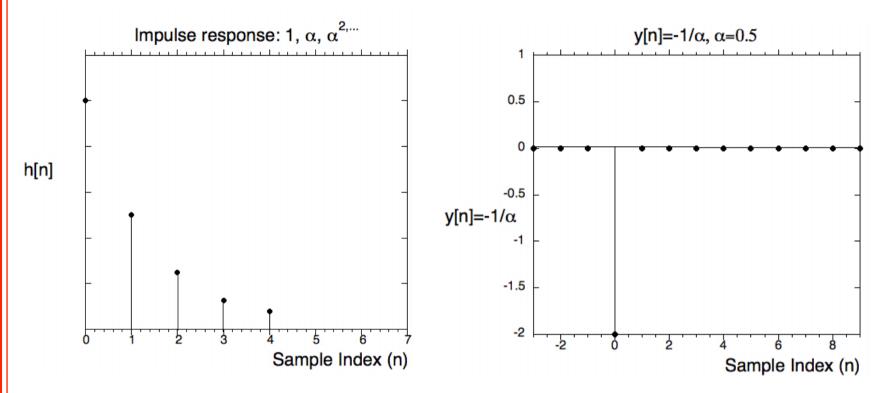
We have that:

$$\Rightarrow Y(Z) = \frac{X(Z) + \alpha . y[-1]}{\left(1 - \alpha . Z^{-1}\right)}$$

$$\Rightarrow Y(Z) = \frac{X(Z) + \alpha \left(-\frac{1}{\alpha}\right)}{\left(1 - \alpha Z^{-1}\right)} = 0$$

i.e., y[n] = 0 for all n > 0!!

What has happened to the signal ? - we had a system with impulse response h[n] = 1, α , α^2 , α^3 , α^4 ,.....



So simply having an initial (prior) condition like $y[n]=-1/\alpha$, the impulse response can be set to zero! The initial (prior) state of the system exactly cancels the impulse response so that the filter output power becomes identically zero!!

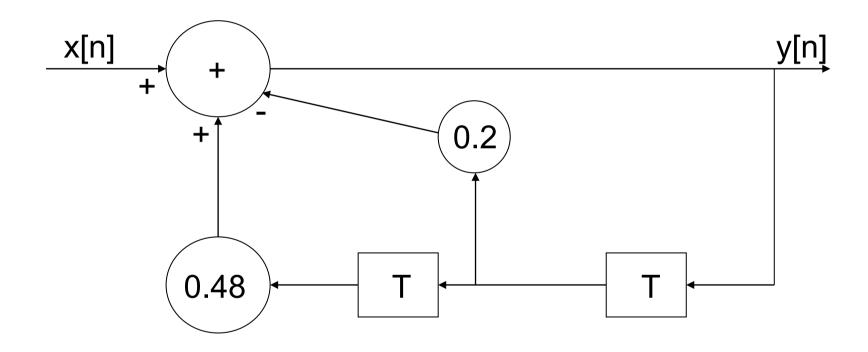
So importantly, h[n] is the impulse response of a processor only if all initial conditions are zero!

i.e., H(Z) = Y(Z)/X(Z) ONLY under zero initial conditions

Problem (for you):

Using
$$y[n] - \alpha .y[n-1] = x[n]$$
 compute h[n] for x[n] = $\delta[n] = 1$ and y[-1] = $1/\alpha$

Example



From the above block diagram we have that: y[n] = -0.2y[n-1] + 0.48y[n-2] + x[n]

Find y[n] when $x[n] = \delta[n]$ for

- (i) Zero initial conditions
- (ii) y[-1] = -1.25 and y[-2] = -0.52083

Taking ZTs of both sides we get for non-zero initial conditions:

$$Y(Z) = \frac{X(Z) - 0.2y[-1] + 0.48y[-2] + 0.48y[-1]Z^{-1}}{1 + 0.2Z^{-1} - 0.48Z^{-2}}$$

Case (i): Zero initial conditions

 $x[n] = \delta[n], \Rightarrow X(Z) = 1 \text{ and } y[n] = h[n] = 0, \text{ for all } y[n] \text{ (n<0)}.$

$$\Rightarrow Y(Z) = \frac{1}{(1+0.2Z^{-1}-0.48Z^{-2})} = \frac{Z^2}{(Z^2+0.2Z-0.48)}$$

$$\Rightarrow Y(Z) = \frac{Z^2}{(Z+0.8)(Z-0.6)} = \frac{AZ}{(Z+0.8)} + \frac{BZ}{(Z-0.6)}$$

Multiply both sides by (Z + 0.8)(Z - 0.6). Values of A & B must be true for all Z. Try poles of Y(Z), i.e., Z = -0.8 & 0.6.

$$\Rightarrow Z^2 = AZ(Z - 0.6) + BZ(Z + 0.8)$$

$$Z = 0.6$$
, $\Rightarrow B(0.6)(1.4) = 0.36$, $\Rightarrow B = 0.4286$
 $Z = -0.8$, $\Rightarrow A(-0.8)(-1.4) = 0.48$, $\Rightarrow A = 0.5714$

Hence
$$\Rightarrow Y(Z) = \frac{0.5714.Z}{(Z+0.8)} + \frac{0.4286Z}{(Z-0.6)}$$

Using table 4.1 on Inverse Z-Transforms we have that:

$$\frac{Z}{Z-a} \to a^n.u[n]$$

$$\Rightarrow y[n] = 0.5714.(-0.8)^n u[n] + 0.4286.(0.6)^n u[n]$$

See figure 4.13(b)

(ii) Non-zero initial conditions: y[-1] = -1.25 & y[-2] = -0.52083

$$Y(Z) = \frac{X(Z) - 0.2y[-1] + 0.48y[-2] + 0.48y[-1]Z^{-1}}{1 + 0.2Z^{-1} - 0.48Z^{-2}}$$

$$Y(Z) = \frac{X(Z) - 0.2[-1.25] + 0.48[-0.52083] + 0.48[-1.25]Z^{-1}}{(1 + 0.8Z^{-1})(1 - 0.6Z^{-1})}$$

$$Y(Z) = \frac{X(Z) + 0.25 - 0.25 - 0.6Z^{-1}}{(1 + 0.8Z^{-1})(1 - 0.6Z^{-1})}$$

$$\Rightarrow Y(Z) = \frac{1}{(1+0.8Z^{-1})} = \frac{Z}{Z+0.8}$$

$$(1+0.8Z^{-1}) \quad Z+0.8$$

$$\Rightarrow y[n] = (-0.8)^n u[n]$$
See figure 4.13(c)